# BEFORE THE HEARINGS PANEL APPOINTED BY CANTERBURY REGIONAL COUNCIL

UNDERthe Resource Management Act 1991 (RMA)ANDIN THE MATTERof an application by Canterbury Regional Council

for resouce consent to discharge agrichemicals to rivers and their connected waterbodies, air and the coastal marine area, and the clearance of vegetation, for the purposes of weed management to provide flood, erosion, drainage and river enhancement works.

### STATEMENT OF EVIDENCE OF Dr Brian Richardson ON BEHALF OF CANTERBURY REGIONAL COUNCIL (APPLICANT)

8 March 2024

### SUMMARY STATEMENT

#### Introduction

- 1 My full name is Brian Richardson. I am employed as a Principal Scientist at the New Zealand Forest Research Institute Ltd operating "Scion" and I have held this position since January 2016.
- 2 I have been asked to undertake modelling, and provide expert evidence, for the Applicant, in regards to quantifying potential drift of agrichemicals when discharged from helicopters.

### **Qualifications and Experience**

- 3 My significant qualifications are:
  - BSc (Hons) Biological Sciences (specialising in Plant Physiology and Ecology), Lancaster University, 1981.
  - MSc (Bio-Aeronautics), Cranfield University, 1982.
  - PhD (Forest Ecology), Oregon State University, 1988.

My MSc focused on the sciences that underpin aerial pesticide spraying technologies. After receiving my MSc, I was employed by the NZ Forest Research Institute (part of the NZ Forest Service) in February 1983 to work on a project to improve the efficiency of aerial herbicide application in forestry. From then until today, I have had many roles but a consistent activity over those 40+ years has been researching aerial spray application with the aim of achieving good management practices that are cost-effectively and environmentally sound.

In the late 1980s I started a collaboration with the US Forest Service, working on an aerial application simulation model they were developing. This model eventually became known as AGDISP, which is the most widely used model of its kind. Some of the contributions to model development and use that I have led or supported include:

- Code checking for first personal computer-based version of the AGDISP (formerly known as FSCBG).
- Collection of field data for model validation.
- Development of first system to integrate model outputs with biological response data to calculate treatment efficacy and environmental impacts.
- Development of first spatial version of AGDISP.

- Sensitivity analysis to develop good practice aerial spraying guidelines for the forest industry.
- During the painted apple moth incursion response, modelling data helped change the entire approach to the response and was used as a treatment guality control tool.
- Evaluation and improvement of the plant canopy deposition model within AGDISP.
- Evaluation of unmanned aerial vehicles as spraying platforms.
- Developing good practice guidelines for aerial spraying to control wilding conifers.
- Many reports using AGDISP modelling have been prepared for clients including MPI, Councils, forestry companies, NZ EPA.

My work has been recognised in various ways e.g.

- Recipient of NZ Plant Protection Medal awarded by NZ Plant Protection Society (2022).
- Science New Zealand lifetime achievement award (2019).
- Superior Paper' Award from the American Society of Agricultural and Biological Engineers (2018; 2019).
- Awarded "Forester of the Year" by NZ Institute of Forestry (2015).
- Numerous invited speaker invitations at science conferences.
- Some refereed science publications related to aerial spray application are listed in Appendix 1.

### Code of Conduct

- I can confirm that I have read and am familiar with the Code of Conduct for Expert Witnesses contained in the Environment Court Practice Note 2023. I have complied with the Code of Conduct in preparing this evidence and I agree to comply with it while giving any oral evidence during this hearing. Except where I state that I am relying on the evidence of another person, my evidence is within my area of expertise. I have not omitted to consider material facts known to me that might alter or detract from the opinions that I express.
- 5 Although I have been contracted by the applicant, I am conscious that in giving evidence in an expert capacity that my overriding duty is to the Hearings Panel.

### Scope of evidence

- 6 I have been asked to provide evidence on behalf of the applicant to inform resource consent applications to discharge agrichemicals and clear vegetation.
- 7 The modelling and my interpretation and recommendations based on those results are included in Attachment 1 which forms the substantive content of my evidence. I have not seen any need to update the recommendations in this report since its preparation and the executive summary follows:

### The problem

8 Canterbury Regional Council (trading as Environment Canterbury) carries out aerial herbicide applications on islands in braided riverbeds to control a range of weed species. Typically, the sprays contain either glyphosate or a mix of glyphosate and triclopyr as active ingredients. With aerial operations there is a risk of off-target spray drift onto sensitive areas beyond the target zone, including water bodies. The purpose of this report was to use the AGDISP spray simulation model to quantify predicted levels of spray drift for a range of spraying scenarios relevant to operational riverbed spraying. Buffer distances (the distance between the spray zone and the sensitive area) needed to avoid unacceptable levels of drift were defined based on the lowest value of the EEL (environmental exposure level) or MAV (maximum acceptable value for drinking water) for herbicide applications using triclopyr or glyphosate plus triclopyr. Model results were used to develop recommendations on buffer zones for herbicide applications in riverbeds.

### **Key results**

Factors having the biggest influence on the buffer zone width needed to ensure herbicide concentrations do not exceed EELs are:

- the choice of nozzle (droplet size),
- wind speed and direction,
- spray release height, and
- the characteristics of the river next to the spray area.

#### **Recommendations**

When spraying weeds in riverbeds, no-spray buffer zones can effectively manage the risk of exceeding acceptable herbicide concentrations in water defined using the environmental exposure limits (EELs).

With the smallest droplet size class tested (coarse spectrum;  $\sim$ 350 µm VMD), a buffer zone of about 10 m is reasonable as long as the flying height is no greater than 3 m above the target vegetation and wind speed is less than 10 km/hr. At greater release heights or windspeeds a buffer of 20 m would be recommended.

With nozzles producing larger drops and a very low driftable fraction (e.g. Accuflo, Thru-valve boom), a buffer zone of 12 m would be adequate for all conditions tested as long as the wind speed does not exceed 15 km/hr. With these nozzles, buffers could be reduced to about 5 m if there is enough confidence that flying height will be less than 3 m above the vegetation and wind speeds in the direction of the water body will be less than 10 km/hr.

Dated 8 March 2024

B Richardse

Brian Richardson

#### Appendix 1: Example Refereed Science Journal Papers on Aerial Spraying

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# Buffer zone estimation to minimise water exposure from aerial spraying with glyphosate or triclopyr

Brian Richardson (Scion) and Wayne Schou (Scion)

March 2023





## **Report information sheet**

Report title Authors	Buffer zone estimation to minimise water exposure from aerial spraying with glyphosate or triclopyr Brian Richardson and Wayne Schou
Client	Canterbury Regional Council
Client contract number	
MBIE contract number	
Scion Report number	64338090
Signed off by	Justin Nairn
Date	March 2023
Confidentiality requirement	
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Published by: Scion, 49 Sala Street, Private Bag 3020, Rotorua 3046, New Zealand. www.scionresearch.com

# **Executive summary**

### The problem

Canterbury Regional Council (trading as Environment Canterbury) carries out aerial herbicide applications on islands in braided riverbeds to control a range of weed species. Typically, the sprays contain either glyphosate or a mix of glyphosate and triclopyr as active ingredients. With aerial operations there is a risk of off-target spray drift onto sensitive areas beyond the target zone, including water bodies. The purpose of this report was to use the AGDISP spray simulation model to quantify predicted levels of spray drift for a range of spraying scenarios relevant to operational riverbed spraying. Buffer distances (the distance between the spray zone and the sensitive area) needed to avoid unacceptable levels of drift were defined based on the environmental exposure level (EEL) for triclopyr, the lowest value of the EEL or MAV (maximum acceptable value for drinking water) for glyphosate and triclopyr. Model results were used to develop recommendations on buffer zones for herbicide applications in riverbeds.

### Key results

Factors having the biggest influence on the buffer zone width needed to ensure herbicide concentrations do not exceed EELs are:

- the choice of nozzle (droplet size),
- wind speed and direction,
- spray release height, and
- the characteristics of the river next to the spray area.

### Recommendations

When spraying weeds in riverbeds, no-spray buffer zones can effectively manage the risk of exceeding acceptable herbicide concentrations in water defined using the environmental exposure limits (EELs).

With the smallest droplet size class tested (coarse spectrum; ~350  $\mu$ m VMD), a buffer zone of about 10 m is reasonable as long as the flying height is no greater than 3 m above the target vegetation and wind speed is less than 10 km/hr. At greater release heights or windspeeds a buffer of 20 m would be recommended.

With nozzles producing larger drops and a very low driftable fraction (e.g. Accuflo, Thru-valve boom), a buffer zone of 12 m would be adequate for all conditions tested as long as the wind speed does not exceed 15 km/hr. With these nozzles, buffers could be reduced to about 5 m if there is enough confidence that flying height will be less than 3 m above the vegetation and wind speeds in the direction of the water body will be less than 10 km/hr.

### Buffer distances to minimise risk of water contamination from wilding conifer aerial herbicide applications

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### Introduction

Aerial herbicide application is a cost-effective treatment for weed control at scale or, when using helicopters or unmanned aerial vehicles (UAVs), in difficult to access locations (Bretthauer, 2015; Richardson, et al., 2017; Richardson, et al., 2019). Canterbury Regional Council uses helicopters for controlling a range of weed species found on islands in braided riverbeds. Typical treatments include glyphosate or a mix of glyphosate, triclopyr and surfactants. Each mix is made up to a total spray volume of 400 L/ha with water.

As with any herbicide application, it is important to ensure that spray drift beyond the target zone is below thresholds of concern for any sensitive areas. Such thresholds can often be defined using published environmental exposure limits (EEL) or maximum acceptable values (MAV) for drinking water standards. However, it can be challenging to quantify drift levels from any spray operation because so many interacting variables influence droplet trajectories when released from an aircraft.

AGDISP (Bilanin, et al., 1989; Teske, et al., 2003) is a mechanistic model that simulates the landing position of droplets released in aerial herbicide applications. A strength of AGDISP is that it includes an aircraft wake model, and it is undoubtedly the most widely used and rigorously tested system of its kind (Bird, et al., 2002; Hewitt, et al., 2002; Teske, et al., 2011). Regulators around the world, including the U.S. Environment Protection Agency, are increasingly relying on AGDISP as part of their regulatory processes. A companion stream assessment model has been incorporated into AGDISP to predict the concentration of aerially applied chemicals in streams adjacent to the sprayed area (Teske, et al., 2002).

Like any model, AGDISP makes many simplifying assumptions and limitations. For example, the model assumes a steady state for meteorological conditions and does not account for variance in meteorological inputs or factors such as aircraft speed or height above the ground. Terrain factors, such as slopes or hills, can have a significant influence on local meteorology but AGDISP does not directly model these effects. While the basic AGDISP model is well-validated within certain constraints, the stream module has had limited validation (Teske, et al., 2002).

Despite the potential limitations when using any complex models such as AGDISP, they can be extremely useful tools for providing operational guidelines and for quantifying the sensitivity or importance of specific variables (Richardson, et al., 2021). The purpose of this report was to quantify the risks of spray drift into streams from a variety of riverbed spraying scenarios relevant to ECAN herbicide application operations.

## **Materials and methods**

### Model scenarios

AGDISP 9.0 was used to quantify spray deposition within and downwind of a spray zone for a range of scenarios as described below. One important point is that all of the scenarios assume that the wind is blowing directly towards a sensitive area, in this case assumed to be a water body. This situation is a worst-case scenario and drift into a sensitive area will be minimal or non-existent if the wind is blowing away from that sensitive area.

A total of 288 spraying scenarios were initially modelled (Tables 1 and 2). Variables that were systematically changed in this sensitivity analysis were spray release height, flying speed, number of flight lines, droplet size, spray mix, and wind speed. Four droplet size spectra were used, characterised according to the volume median diameter (VMD). From smallest to largest, these sizes were representative of the follow standards classes according the ASABE (American Society of Agricultural and Biological Engineers Classification): Coarse (353  $\mu$ m), Ultra Coarse (> 650  $\mu$ m), and two classes exceeding Ultra Coarse (785, 958  $\mu$ m).

Input variable	Value
Aircraft and spray block:	
Aircraft type	AS 350, B2 3A
Release height above vegetation	3 m, 5 m
canopy of 3 m	
Aircraft speed	30, 50 knots; (15.4, 25.7 m/s)
Nominal lane separation	4 m
Number of flight lines	3, 12, 20
Application technique:	
Nozzie location	Distributed evening to 80% rotor diameter i.e. a boom
) (aluma median diamatan () (MD)	width of approximately 8.5 m
	$\sim$ 353, 659, 765, 956 µm (see Appendix 1 for details)
Meteorology (2 m reference ht):	
Wind speed	5, 10, 15 km/hr (1.39, 2.78, 4.17 m/s)
Wind direction (relative to flight lines)	Crosswind (-90°)
Temperature	22
Relative humidity	75
Atmospheric stability	Overcast
Canopy:	
Height	3 m

 Table 1: Baseline and variable AGDISP inputs.

Two spray mixes were used in the simulations (Table 2), one containing only glyphosate and the other a mix of glyphosate (at the same rate as glyphosate alone) and triclopyr plus adjuvants. Both spray mixes were applied at a total spray volume of 400 L/ha.

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	Spray mix 1	Spray mix 2
Active ingredient	Glyphosate	Glyphosate (G) + triclopyr (T)
Product rate	7 L/ha	7 L/ha (G) + 2 L/ha (T)
Active ingredient (AI) rate	7 x 0.49 = 3.43 kg/ha	7 x 0.49 = 3.43 kg/ha (G) + 2 x 0.60 = 1.20 kg/ha (T)
Adjuvants	-	2 L/ha Excel oil or an organosilicone surfactant
Total spray volume	400 L/ha	400 L/ha
Active fraction	0.00858	0.01158
Non-volatile fraction	0.0175	0.0275

### Modelled spray deposition, threshold definition and buffer distances

For each of the scenarios (all combinations of variables in Table 1), spray deposition was modelled within and downwind of the target area (Figure 1). Buffer distances were all referenced from the flight line i.e. the centre of the aircraft.



**Figure 1.** Overlapped swaths from 3 flight lines are summed to give total deposition both within and downwind of the spray block. Estimation of a suitable buffer distance depends on defining an acceptable threshold value of off-site deposition.

Spray deposition typically attenuates rapidly with distance downwind of the spray area. However, small quantities of herbicide may still be deposited at large distances downwind. The question is how to define a level of deposition that is biologically insignificant in terms of the risks being managed. One option is to use published thresholds, such as the Maximum Acceptable Values (MAV) for drinking water standards and Environmental Exposure Limits (EELs) (Table 3). As EELs have a consistently lower acceptable concentration than MAVs for these herbicides (i.e. you can exceed an EEL without exceeding a MAV), EELs were used here as the threshold values for defining acceptable and unacceptable herbicide concentrations. Using the EEL threshold value, buffer distances were calculated for each model run. This buffer distance represents the distance required between the most downwind flightline and the sensitive area to ensure that the EEL value is not exceeded in the sensitive area.

Herbicide	MAV (mg/L)	EEL (mg/L)		
Triclopyr	0.1	0.059		
Glyphosate	0.9	0.37		

**Table 3:** Maximum acceptable values (MAV) for drinking water standards and EnvironmentalExposure Limits (EELs) for glyphosate and triclopyr (active ingredient values).

As the AGDISP simulations calculate deposition as an amount per unit area, a method is required for converting the area-based deposition to a concentration if we are to use the EEL values as thresholds. <u>Hence, it was assumed that spray was deposited on to a static water body of 1 m depth to enable conversion of the deposition data to a concentration.</u> If it is assumed that the nominal application rates were deposited on the static water body, it would represent a concentration of over twice the EEL value for triclopyr but about 7% below the EEL value for glyphosate. For this reason, the analysis primarily focused on generating buffer distance requirements for triclopyr as the worst-case scenario.

### Moving water body

Once the primary analysis was completed using the 1 m static water body to define herbicide concentrations, a small number of additional model runs (16) were carried out using the stream model in AGDISP (Figure 2). The stream assessment model considers:

- The spray line length (assumed to run parallel to the stream).
- Turnaround time (how long it takes the pilot to change from spraying one flight line to the next).
- Stream width, depth and flow rate.
- Distance from the edge of the application area to the centre of the stream.

- Riparian interception factor (an index of the amount of active material removed from the air by vegetation growing upwind of the stream but downwind of the sprayed area).
- Instream chemical decay rate (assumed to be negligible in this analysis).
- Recharge rate the flow rate per unit distance downstream for fresh water entering the stream.





Details of the stream model inputs are summarised in Tables 4 and 5.

Input variable	Value						
Spray line length (parallel to stream) (m)	100						
Number of flight lines	12						
Helicopter turn-around time (s)	20						
Riparian interception factor	0.0						
Instream chemical decay rate (1/day)	0						
Recharge rate (m³ s⁻¹ km⁻¹)	0						
Distance (m) from edge of spray block to stream centre	Based on buffer calculated in main analysis						
Sampling location (m)	50 m						

Table	4:	Stream	factor	model	inputs
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	Scenario 1	Scenario 2	Scenario 3	Scenario 4
Stream width	2 m	5 m	25 m	200m
Stream depth	0.5 m	1 m	1 m	2 m
Flow rate	1.0 m³/s	1.88 m³/s	50 m³/s	300 m³/s
Flow speed	1.0 m/s	0.376 m/s	2 m/s	0.75 m/s

 Table 5: Modelled stream scenarios

### Data analysis

Using the triclopyr data as the worst-case scenario, summary statistics were generated for the key variables in the analysis to quantify their sensitivity in terms of buffer distance requirements. Subsequently, the interactions between most sensitive variables were graphed to visualise buffer requirements for a range of scenarios.

The buffer distances calculated for a small number of scenarios (16) were inserted into the stream model for each of the stream scenarios (Table 5). The calculated herbicide concentration for each stream scenario was compared with the EEL value to determine whether the buffer estimated for the static water (baseline) scenario was sufficient for achieving below-EEL concentrations across all of the stream scenarios.

### **Results and Discussion**

### Sensitivity analysis

As expected from many previous analyses, the variables droplet size, wind speed and spray release height had the biggest influence on the distance needed (i.e. the buffer distance) between the downwind flightline (measured from the centre of the aircraft) and a sensitive area to ensure triclopyr values would be below EEL values (Figures 3 - 5). Of these variables, wind speed gave the greatest range in buffer distance, from 4.9 to 10.5m. However, it should be noted that all of the droplet spectra were made up of relatively larger droplet sizes with volume median diameters VMD's ranging from 353 to 958 µm.



Figure 3. Buffer distance for each VMD (droplet size), averaged across all other factors.



Figure 4. Buffer distance for each wind speed, averaged across all other factors.



Figure 5. Buffer distance for each release height, averaged across all other factors.

The other variables evaluated, including the number of flight lines and flying speed had a relatively small effect on buffer distance (Figure 6). While the most downwind flight line has the potential to make the greatest contribution to stream deposition because of its proximity, successive flight lines also have the potential to add additional spray deposition to the stream. However, with the relatively large droplet sizes used in all cases, this variable only had a minor effect on buffer distance.

While this analysis did not test the sensitivity of other variables, such as temperature and humidity, previous analyses have shown that they were unlikely to have had a major effect on buffer distance within the ranges of relevance to these scenarios.



Figure 6. Buffer distance for each number of spray lines and flying speed.

### Interactions among the three key variables

The effects of droplet size, wind speed, and spray release height on buffer distance, averaged across other factors, are summarised in Figures 7 and 8. With the smallest droplet VMD tested (353  $\mu$ m) and the highest wind speed, the required buffer distance ranged from 11.1 m to 17.4 m for the 6 m and 8 m spray release heights (i.e. 3 m and 5 m above vegetation canopy of 3 m), respectively. At the lowest wind speed tested but for the same droplet size, buffer distances reduced to between 5.6 and 8.0 m for the 6 m and 8 m spray release heights, respectively.



Figure 7. Effect of wind speed and droplet size on buffer distance for a 6 m release height.



Figure 8. Effect of wind speed and droplet size on buffer distance for an 8 m release height.

At the other end of the droplet size scale, there was little difference in buffer distances required for the two larger droplet size classes, primarily because they had very similar driftable fractions (volume of spray in droplets less than 150  $\mu$ m). For these droplet sizes,

buffer distances ranged from 3.1 m for the lowest wind speed and release height to 10.8 m for the strongest wind and greatest spray release height.

### Comparison of results with the stream model

The results presented above are all predicated on the calculated concentration of triclopyr deposited in a 1 m deep static water body. If the same analysis was undertaken assuming a different static water volume e.g., a 0.5 m deep static water body, the results would have shown a requirement for greater buffer distances. To evaluate whether the results are reasonable for real operational situations, results were compared with stream simulations as described in Tables 4 and 5. A caveat to this analysis is that the AGDISP stream model has had little validation and testing. If the results from this analysis are deemed useful, it is recommended that a more rigorous evaluation of the stream model is carried out.

Using a 1 m deep static water body as a baseline for converting spray deposition data to herbicide concentrations generated buffer distances that provided protection for 13 out of 16 stream scenario/spray method combinations tested (Table 6). The main exception was stream scenario 1, the shallowest stream scenario, where there were two EEL exceedances. For the three cases where there were EEL exceedances, implementing a 10 m buffer would have provided adequate protection (Table 7).

stream	stream scenarios. Coloured boxes indicate: red = exceedance of EEL; green = below EEL.								
Wind Air Buffer Herb							le (mg/L) f	or stream	scenario
(μm)	Height (m)	Spray Lines	speea (m/s)	speea (m/s)	(baseline) (m)	1	2	3	4
785	6	12	1.39	15.43	3.52	0.2297	0.0757	0.0069	0.0001
785	8	12	4.17	25.72	11.72	0.0328	0.0113	0.0012	0.0000
353	6	12	1.39	15.43	5.31	0.0762	0.0391	0.0047	0.0001
353	8	12	4.17	25.72	18.73	0.0289	0.0167	0.0024	0.0001

**Table 6:** Calculated peak herbicide concentrations for all combinations of 4 AGDISP runs and 4 stream scenarios. Coloured boxes indicate: red = exceedance of EEL; green = below EEL.

<b>Table 7:</b> Buffer distances that provide protection for all stream scenarios.	Green coloured boxes
indicate herbicide concentrations below the EEL threshold.	

	Usiabt	Correct	Wind	Air	Undeted -	Herbicide (mg/L) for stream scena			scenario
(μm)	meight (m)	Spray Lines	speed (m/s)	speed (m/s)	buffer (m)	1	2	3	4
785	6	12	1.39	15.43	10	0.0085	0.0041		
353	6	12	1.39	15.43	10	0.0334			

Water concentrations are reduced with wide, deep and fast flowing rivers. The model averages overall herbicide concentration across the entire water body. Where the river is wide, the amount of spray deposited into the upwind edge of the river will be much higher than the downwind edge. Hence, although the overall result reported represent an average peak concentration across that width, the actual peak value at the upwind edges will be higher than reported.

### **Results with glyphosate**

Results with glyphosate have not been shown because even a direct overspray of glyphosate into a water body, as described in the Methods section, will not result in EEL exceedance. Nevertheless, drift mitigation options described below will still ensure minimal stream contamination occurs.

### **Droplet size selection**

A key decision influencing the width of buffer zone, regardless of other conditions is droplet size. The VMD of a droplet spectrum is usually inversely related to the driftable fraction, the total spray volume in droplets less than about 150 µm i.e. the larger the VMD, the lower the driftable fraction. Going to large droplet sizes significantly reduces the driftable fraction and the buffer distance requirement but using larger droplets can also have down sides. For example, more accurate flying is needed with large drops because of the steep cut-off to swath patterns. Further, herbicide efficacy is often related to the degree of coverage on the target plant, especially when using poorly translocated herbicides such as triclopyr (glyphosate by contrast is generally well translocated). Target coverage will decrease as droplet size increases (at least within the limits described in this report), hence there is an incentive to use smaller droplets from an efficacy perspective. By contrast, as shown by the results of this analysis, the potential for drift also increases with smaller drops, requiring larger buffer distances.

Droplet size is influenced by a wide range of factors including:

- Type and size (flow rate) of nozzle.
- Nozzle orientation relative to the flight direction.
- Spraying pressure.
- Air speed.
- Spray formulation physical properties.

It is very difficult to predict droplet sizes because of all of these interacting factors. However, there are good sources where droplet size information can be accessed. Manuals produced by nozzle manufacturers generally classify nozzles according to the droplet spectrum they produce. While this information is useful for the relative performance of different nozzles, it has limited value for aerial spraying because the manuals generally assume the applications are from ground sprayers and do not include the important effects of nozzle orientation, air speed and formulation. However, there are a number of publications and online sources with databases of droplet spectra measurements relevant to aerial application e.g. (MPI, 2022; Richardson, et al., 2020).

### Managing risk of stream contamination

The AGDISP analysis presented here is based on a worst-case scenario with the assumption of steady-state meteorology including a constant wind speed blowing towards the sensitive area (water body). Good practice for aerial application dictates that spraying should only take when the wind is blowing away from any sensitive areas. If this principle is followed, the risk of water body contamination is low and should only occur if there are sudden wind shifts or unexpected local wind flows. However, it is not always possible to spray with the wind blowing away from the sensitive area, especially if spraying an island in a riverbed surrounded by water or if meteorological conditions suddenly change during an operation.

Results from this study, based on the triclopyr EEL and assuming the water body conditions are as described in the Methods, indicate that the risk of water body contamination from aerial spraying can be managed through implementation of buffer zones i.e. no spray zones between the sprayed area and water body to be protected. The width of the buffer zone needed to ensure any spray deposition into water results in concentrations below EEL values depends on the characteristics of the spray application and of the water body.

A key decision influencing the width of buffer zone is the choice of nozzle and droplet size. With the smallest class tested, a buffer zone of about 10 m is reasonable as long as the flying height is no greater than 3 m above the target vegetation and wind speed is less than 10 km/hr. At greater release heights or windspeeds a buffer of 20 m would be recommended.

With nozzles producing a very low driftable fraction (e.g. Accuflo, Thru-valve boom) a buffer zone of 12 m would be adequate for all conditions tested as long as the wind speed does not exceed 15 km/hr. Buffers could be reduced to about 5 m if there is enough confidence that flying height will be less than 3 m above the vegetation and wind speeds in the direction of the water body will be less than 10 km/hr.

It is important to note that all situations are different and weather conditions are dynamic so these recommendations cannot be taken as absolute. Other factors that reduce spray drift risk could also be considered when making decision on buffer zone width including the presence of vegetation hanging over the water (captures spray that would otherwise be deposited in the water), and rivers that are wide, deep and fast flowing.

# Conclusions

When spraying weeds in riverbeds, no-spray buffer zones can effectively manage the risk of exceeding acceptable herbicide concentrations in water defined using the environmental exposure limits (EELs). Factors having the biggest influence on the buffer zone width needed to ensure herbicide concentrations do not exceed EELs are:

- the herbicide type and EEL,
- the choice of nozzle (droplet size),
- wind speed and direction,
- spray release height, and
- the characteristics of the river next to the spray area.

Use of nozzles that produce a low driftable fraction (e.g. Accuflo, Thru-valve booms) significantly reduce the risk of exceeding EEL values. However, for the triclopyr herbicide mix, buffers of between 5 and 20 m, depending on the spray operational and river characteristics, can provide adequate protection with a coarse droplet spectrum and within the meteorological and operational limits defined in this study.

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Medium Co 35	Medium Coarse (VMD = 353µm)		Ultra Coarse (VMD = 659µm)		Accuflo (VMD =785um	
Upper size (µm)	Cumulative % volume	Upper size (µm)	Cumulative % volume	Upper size (µm)	Cumulative % volume	
40.57	0.100	68.62	0.310	36	0.000	
47.03	0.200	105.11	0.730	44	0.000	
54.50	0.400	143.14	1.470	52	0.000	
63.16	0.800	182.76	2.670	62	0.000	
73.23	1.300	224.06	4.460	74	0.000	
84.85	1.800	267.09	6.950	86	0.000	
98.12	2.500	311.93	10.230	100	0.000	
113.71	3.700	358.66	14.340	120	0.000	
131.73	5.800	407.36	19.280	150	0.000	
152.79	8.700	458.11	25.010	180	0.000	
177.84	11.850	510.99	31.450	210	0.000	
205.84	15.600	566.10	38.460	250	0.050	
238.45	21.800	623.52	45.810	300	0.140	
276.48	30.450	683.37	53.190	360	0.330	
320.60	42.200	745.73	60.500	420	0.570	
372.18	55.350	810.71	67.450	500	1.340	
430.74	68.500	878.43	73.820	600	6.480	
498.91	80.400	949.00	79.470	720	32.230	
578.54	89.250	1022.54	84.340	860	74.360	
670.72	93.350	1099.18	88.410	1020	97.300	
777.39	95.100	1179.04	91.690	1220	99.570	
900.61	96.550	1262.26	94.240	1460	99.570	
1044.42	97.800	1348.98	96.140	1740	99.970	
1210.66	99.000	1439.35	97.500	2060	100.000	
1403.04	100.000	1533.53	98.430	2460	100.000	
		1631.67	99.040	2940	100.000	
		1733.93	99.430			
		1840.51	99.660			
		1951.56	99.800			
		2067.29	100.000			

### Appendix 1 – Droplet spectrum information

Upper size         Cumulative % volume           40.50         0.000           46.83         0.000           54.33         0.000           54.33         0.000           63.00         0.000           73.00         0.000           84.67         0.000           98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050           1041.67         57.870           1206.67         71.540           1400.00	TVB (VN	TVB (VMD =958µm)				
Size         Cumulative           (µm)         % volume           40.50         0.000           46.83         0.000           54.33         0.000           63.00         0.000           73.00         0.000           84.67         0.000           98.17         0.010           113.67         0.030           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	Upper	Cumulativa				
40.50         0.000           46.83         0.000           54.33         0.000           63.00         0.000           73.00         0.000           73.00         0.000           84.67         0.000           98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	(µm)	% volume				
46.83         0.000           54.33         0.000           63.00         0.000           73.00         0.000           84.67         0.000           98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	40.50	0.000				
54.33         0.000           63.00         0.000           73.00         0.000           84.67         0.000           98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	46.83	0.000				
63.00         0.000           73.00         0.000           84.67         0.000           98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050 <th>54.33</th> <th>0.000</th>	54.33	0.000				
73.00         0.000           84.67         0.000           98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	63.00	0.000				
84.67         0.000           98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	73.00	0.000				
98.17         0.010           113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	84.67	0.000				
113.67         0.030           131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	98.17	0.010				
131.83         0.060           152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	113.67	0.030				
152.83         0.110           176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	131.83	0.060				
176.67         0.200           205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	152.83	0.110				
205.00         0.350           238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	176.67	0.200				
238.33         0.640           275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	205.00	0.350				
275.00         1.210           320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	238.33	0.640				
320.00         1.940           370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	275.00	1.210				
370.00         2.870           430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	320.00	1.940				
430.00         4.780           498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	370.00	2.870				
498.33         8.680           576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	430.00	4.780				
576.67         14.990           668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050           100         100.050	498.33	8.680				
668.33         23.420           775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	576.67	14.990				
775.00         33.580           898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	668.33	23.420				
898.33         45.200           1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	775.00	33.580				
1041.67         57.870           1206.67         71.540           1400.00         85.630           1621.67         100.050	898.33	45.200				
1206.67         71.540           1400.00         85.630           1621.67         100.050	1041.67	57.870				
1400.00         85.630           1621.67         100.050	1206.67	71.540				
1621.67 100.050	1400.00	85.630				
	1621.67	100.050				